



Discrete vs. smeared modelling of rock slopes or where are the application limits of the Hoek-Brown strength criterion.

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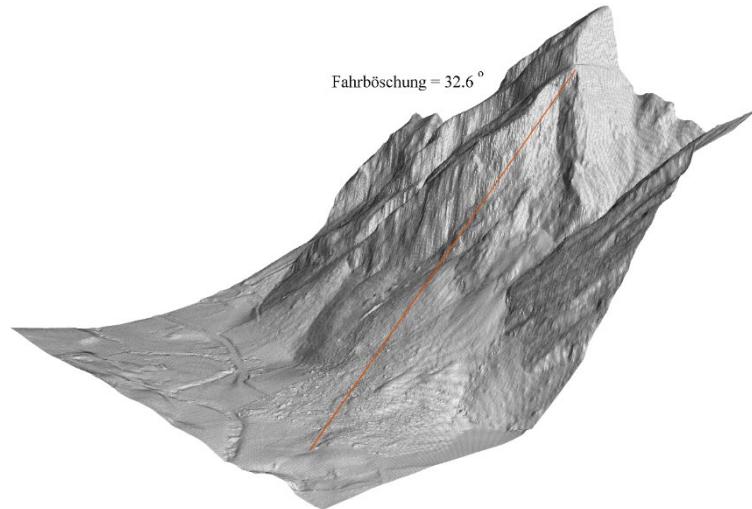
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Example Rock Fall Vals



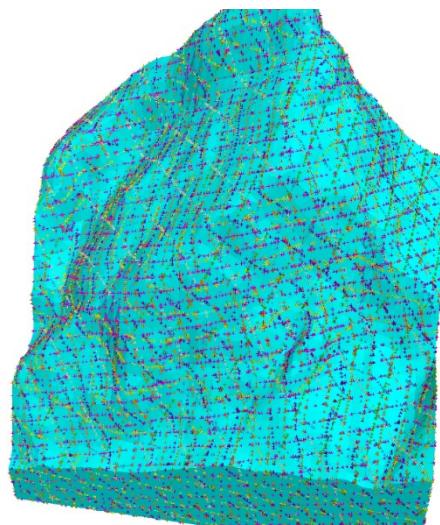
Geology Valsertal: Part of the Tauern window; mostly hard and firm calcareous marbles and calcareous mica schists (UCS > 100 MPa, class R5 according to ISRM 1981), subordinate also low-strength calcareous phyllites and graphite pyllites.

Research Project

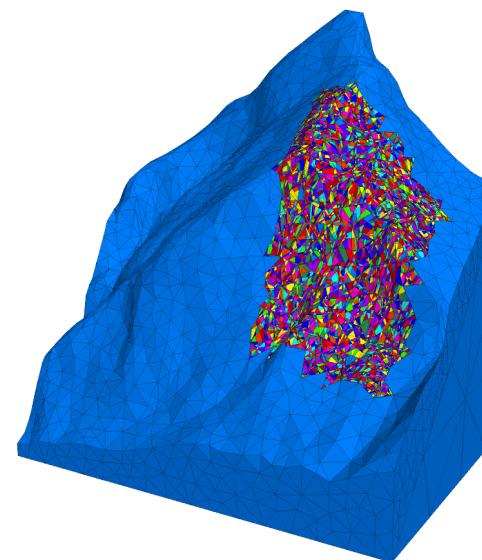
FEM or FDM



Conventional DEM

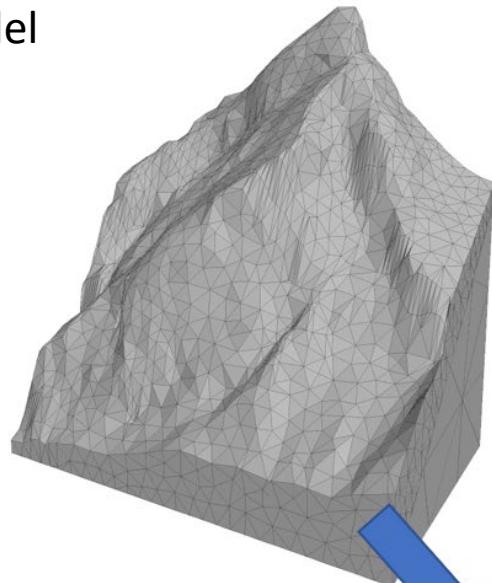


DEM using a Synthetic Rock Mass (SRM)

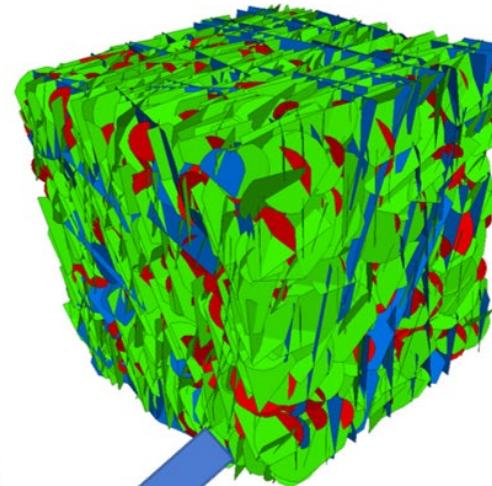


Methodology Synthetic Rock Mass (SRM)

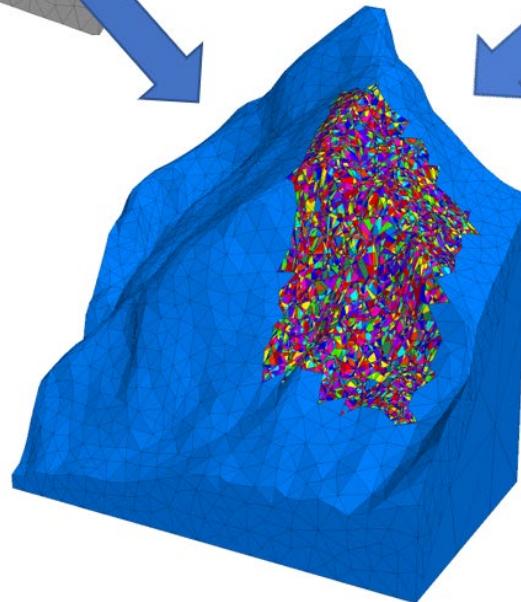
Solid model



Discrete Fracture Network (DFN)



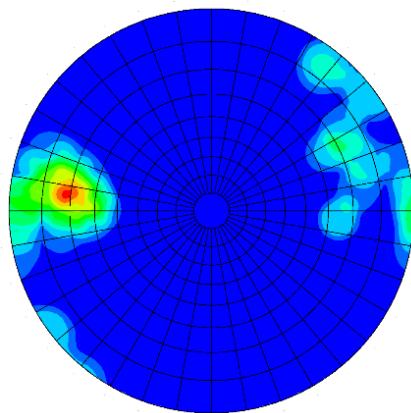
SRM



- Position
- Orientation
- Fracture Size Distribution
- Density or Fracture Intensity

Discrete Fracture Network (DFN)

Orientation

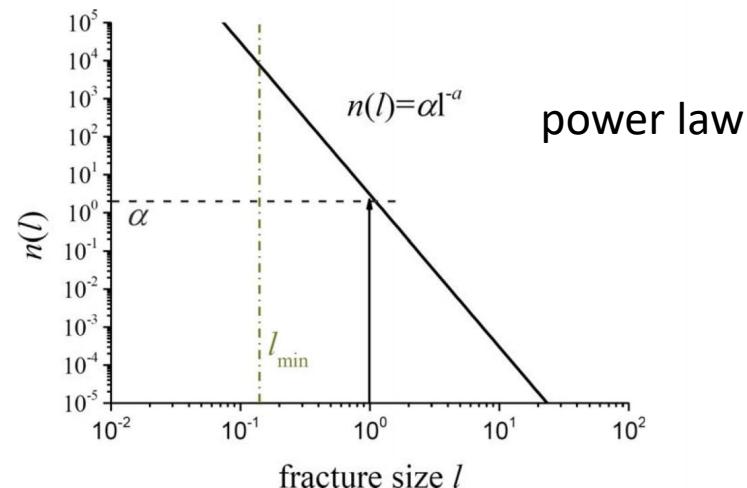


e.g. Fisher

fracture density

		Dimension of Feature				
		0	1	2	3	
Dimension of Sample	Line	P_{10} Number of fractures per unit length [m^{-1}]	P_{11} Fracture aperture per unit length [-]			Linear Measures
	Area	P_{20} Number of fractures per unit area [m^{-2}]	P_{21} Length of fractures per unit area [m^{-1}]	P_{22} Area of fractures per unit area [-]		Areal Measures
	Volume	P_{30} Number of fractures per unit volume [m^{-3}]		P_{32} Area of fractures per unit volume [m^{-2}]	P_{33} Volume of fractures per unit volume [-]	Volumetric Measures
		Density	Intensity	Porosity		

Fracture Size Distribution



power law

DFN

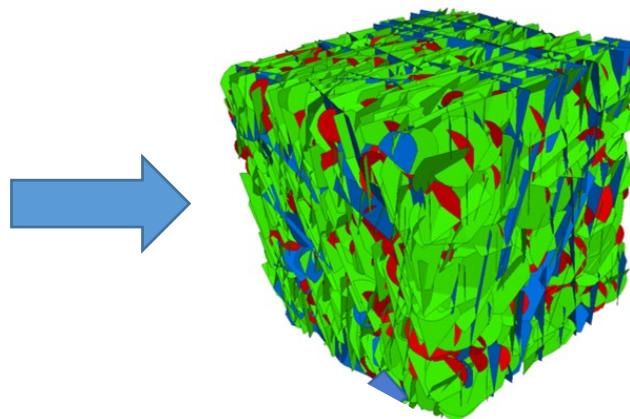


Table 6.1 Summary of parameters used to generate the three fracture sets

Fracture set	Property	Distribution	Parameters
set 1: subvertical	positions	uniform	positions generated in all of space
	orientations	Fisher	dip 90° , dip direction: 120° , $\kappa = 200$
	lengths	power law	scaling exponent: $a = 4$, $l_{min} = 10$, $l_{max} = 500$
	density		$P_{32} = 0.33$ in the model domain extent
set 2: subhorizontal	positions	uniform	positions generated in all of space
	orientations	Fisher	dip 20° , dip direction: 30° , $\kappa = 500$
	lengths	power law	scaling exponent: $a = 4$, $l_{min} = 10$, $l_{max} = 500$
	density		number of observed fractures on the vertical outcrop: 39
set 3: background	positions	uniform	positions generated in all of space
	orientations	bootstrapped	from file
	lengths	power law	scaling exponent: $a = 3.2$, $l_{min} = 2$, $l_{max} = 10$
	density		P_{10} measured on the vertical borehole of length 85 m: 0.5

Intact rock parameters from laboratory tests

Intact rock

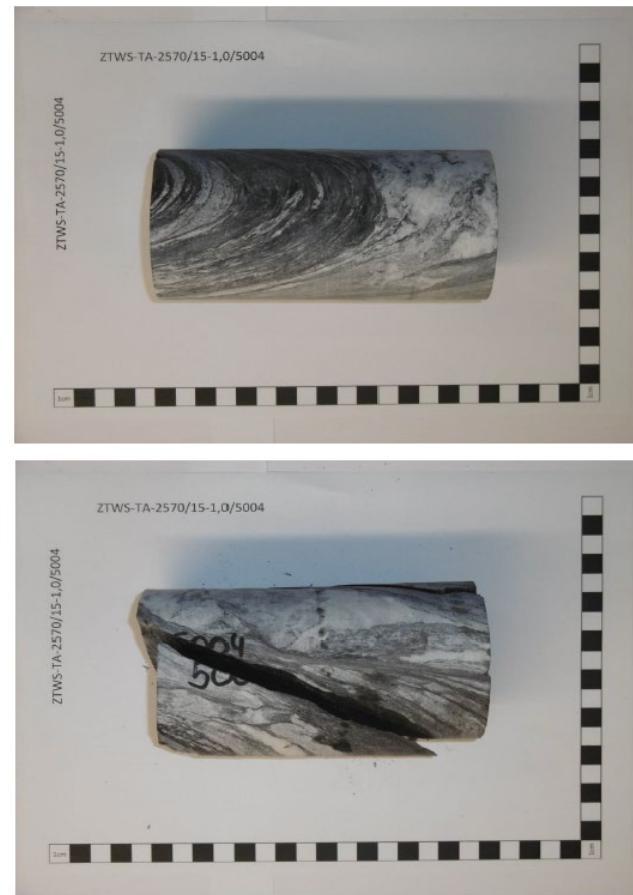
Density
Young's modulus
Poisson's ratio

Friction angle
Cohesion
Tensile strength

Joints

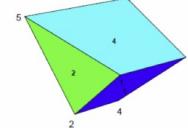
Normal stiffness
Shear stiffness

Friction angle
Cohesion
Tensile strength

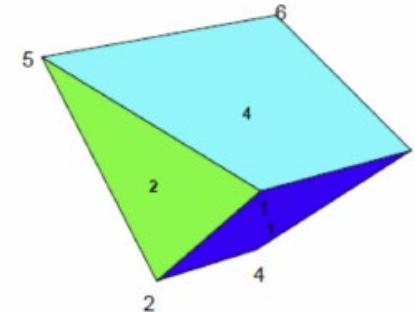


Due to the high computation times, density upscaling is required.

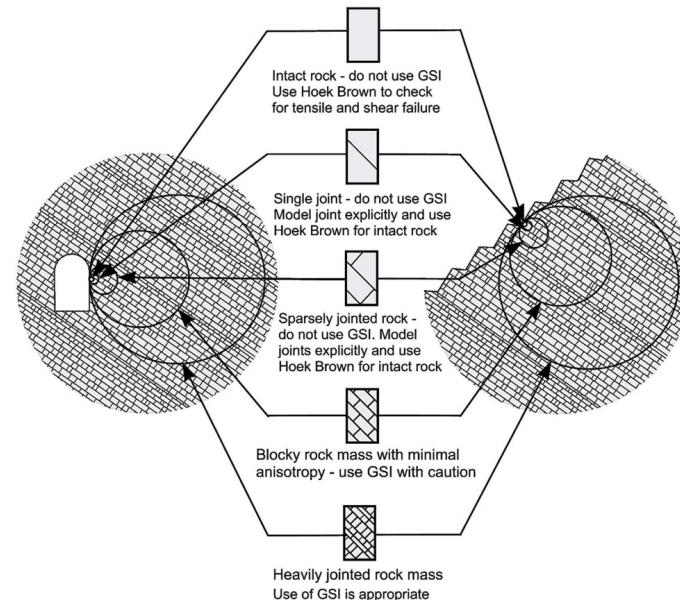
Laboratory scale



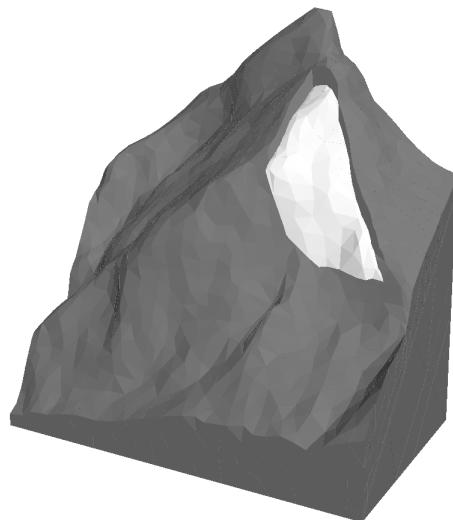
Model scale



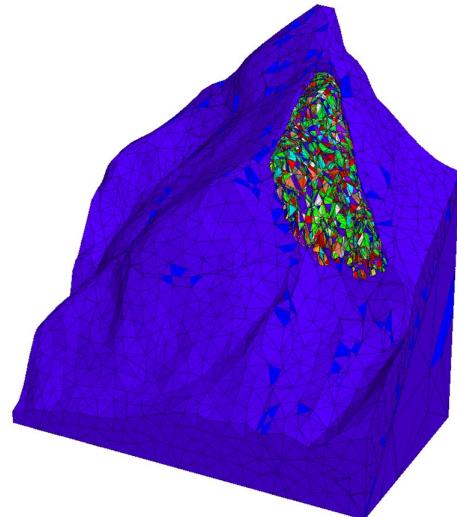
The blocks become larger than they are in situ!



Back-calculating the failure



Model A: Rigid Wedge

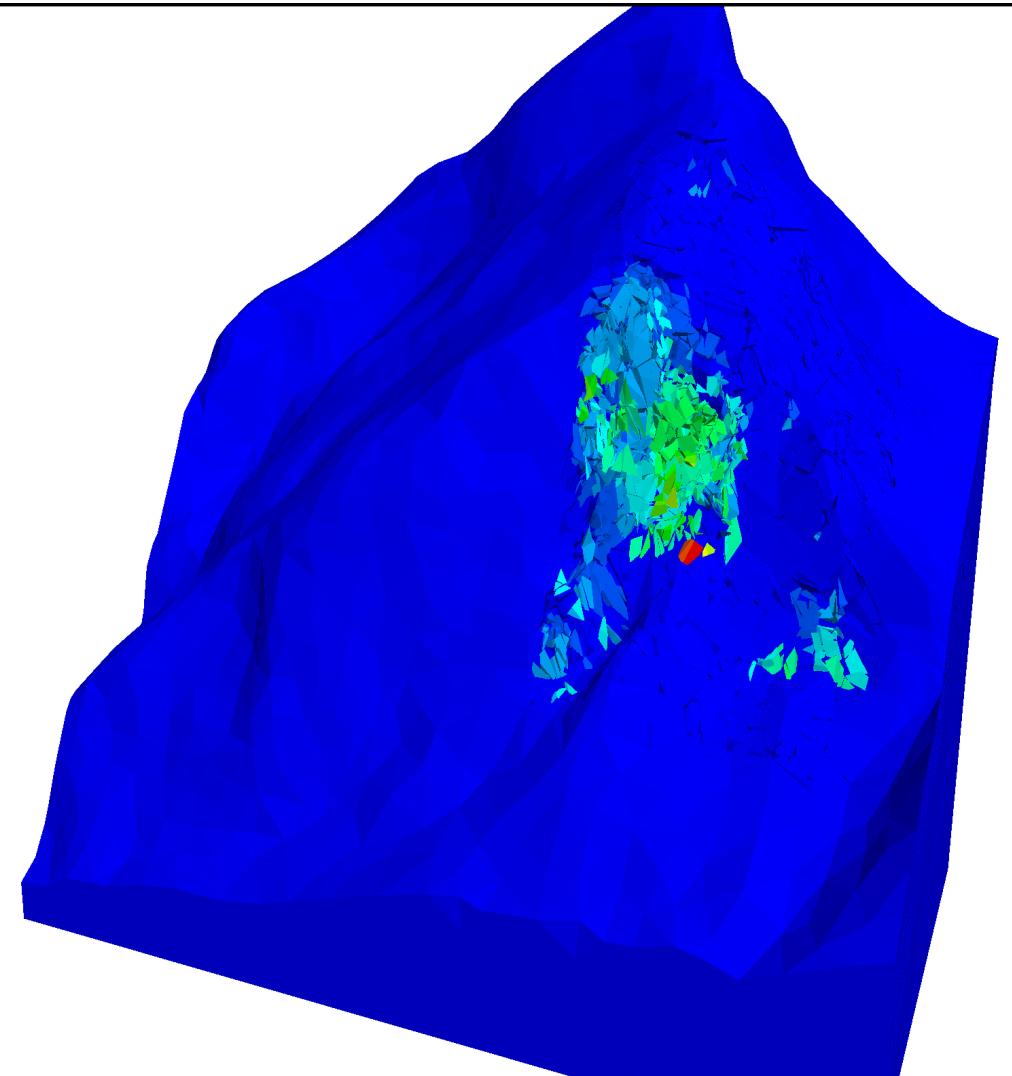
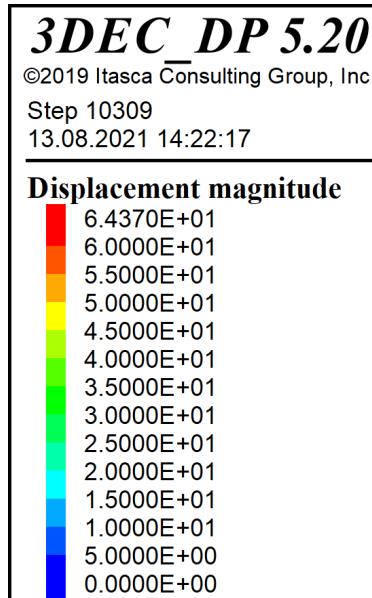


Model C: Wedge discretized via SRM

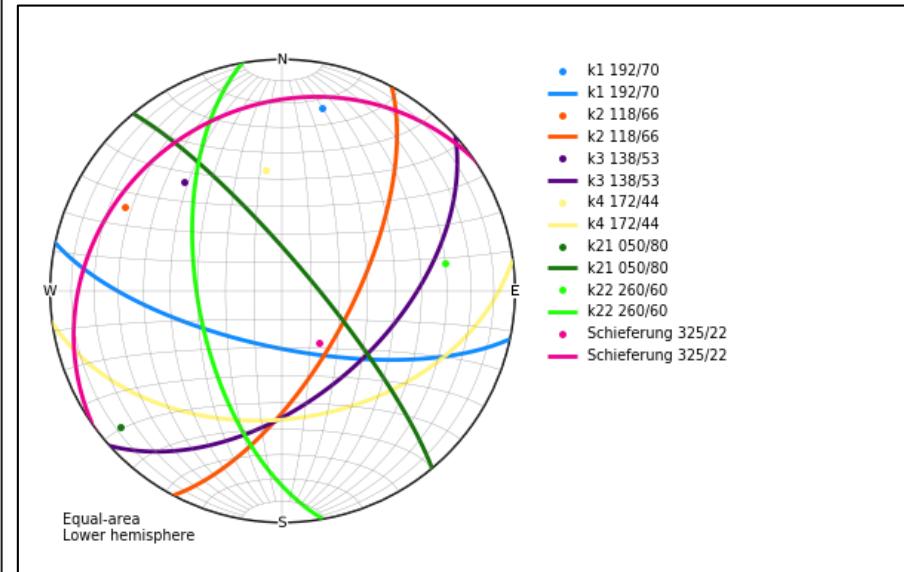
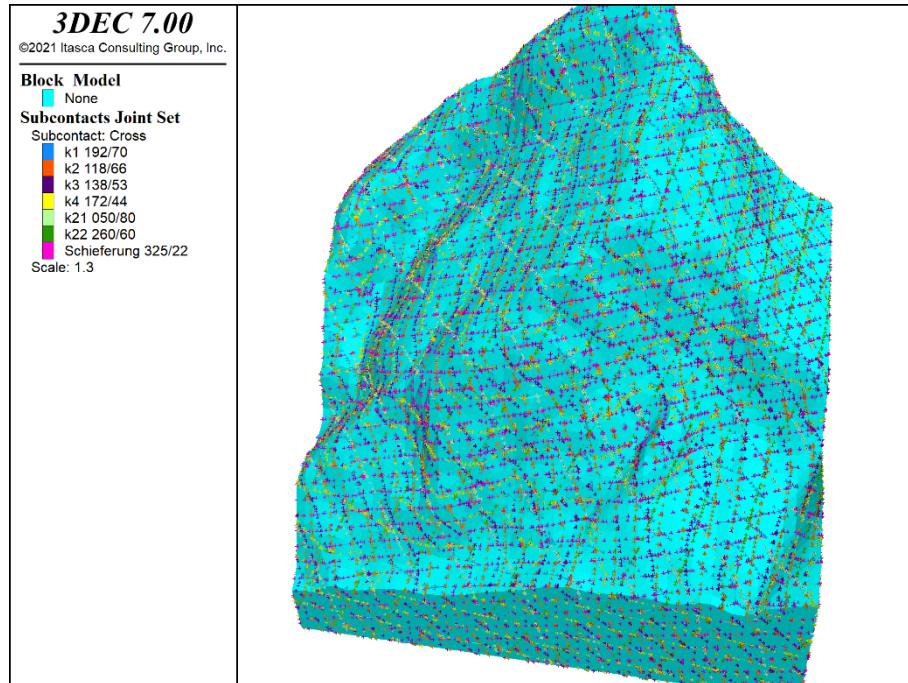
Fracture Intensity vs. Factor of Safety

<u>Versuch Nr.</u>	$I_{\text{new}} / I_{\text{start}}$	FoS
Versuch_1b_1	1/20	0,4
Versuch_1b_2	1/40	0,4
Versuch_1b_3	1/80	0,6
Versuch_1b_4	1/100	0,8

Deplacements - rigid block model

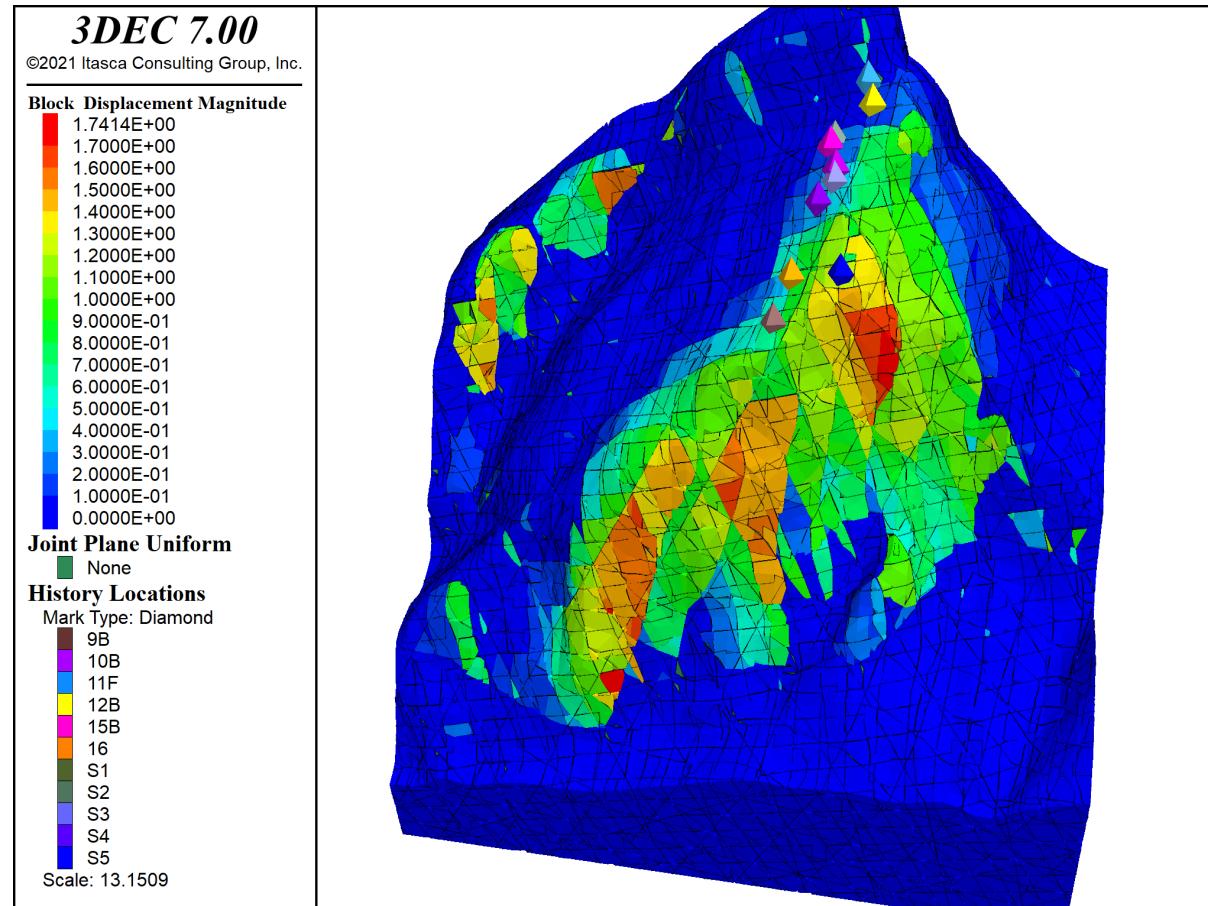


Conventional DEM: taking into account the mean orientations of the discontinuities.



Interface strengths from wedge analysis

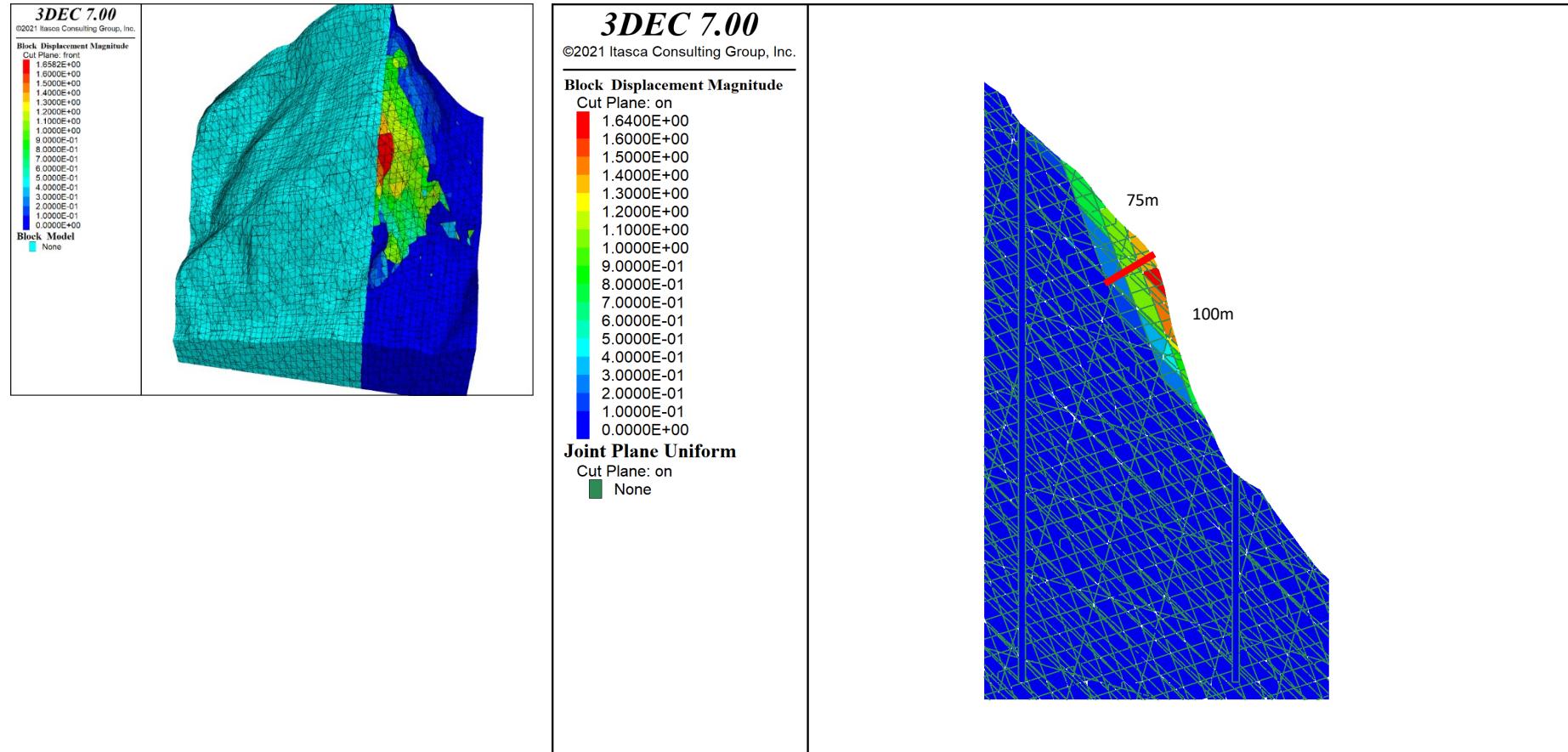
$$\varphi_{\text{grenz}} = 42,3^\circ, c_{\text{grenz}} = 0,5 \text{ MPa.}$$



Contour plot of displacement magnitudes [m], 20,000 calculation steps

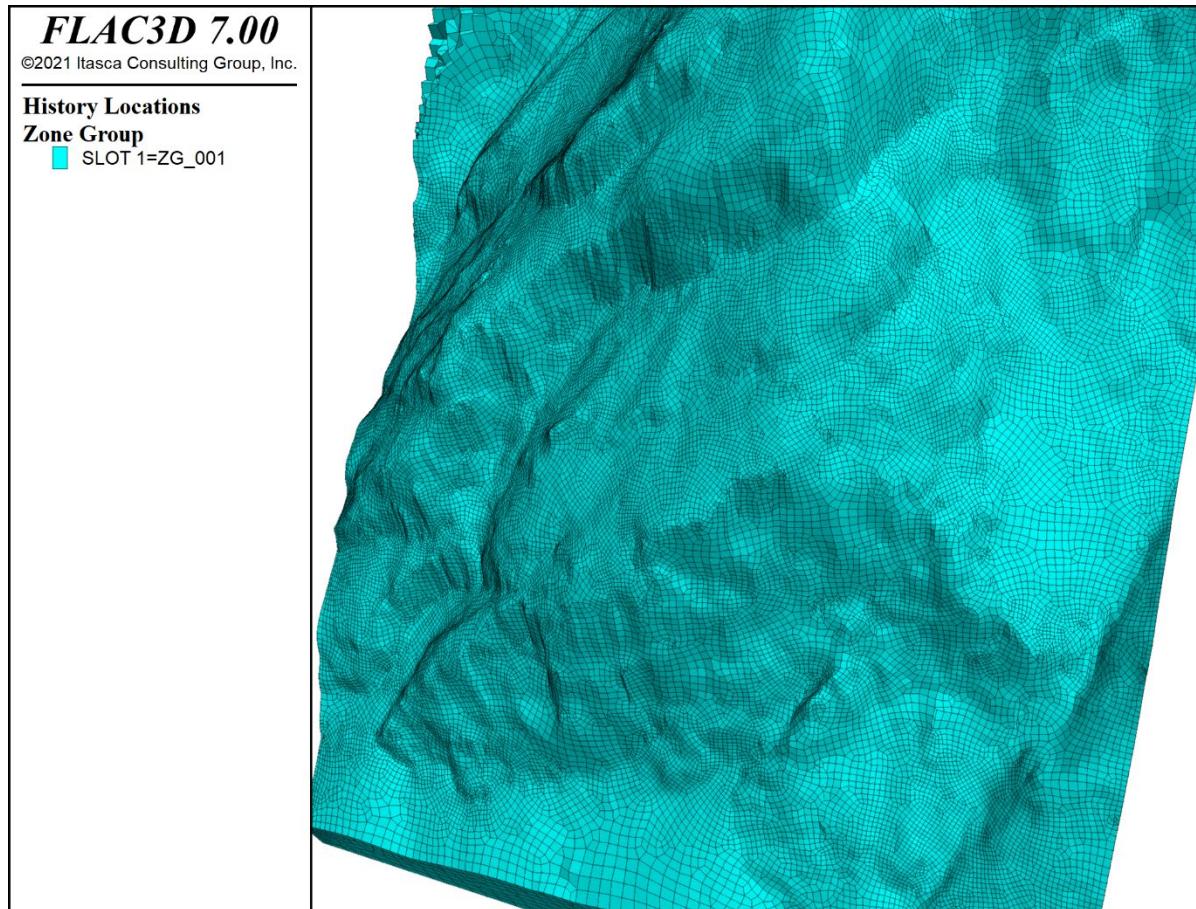
Rigid block model

Depth of movement: ca. 30m



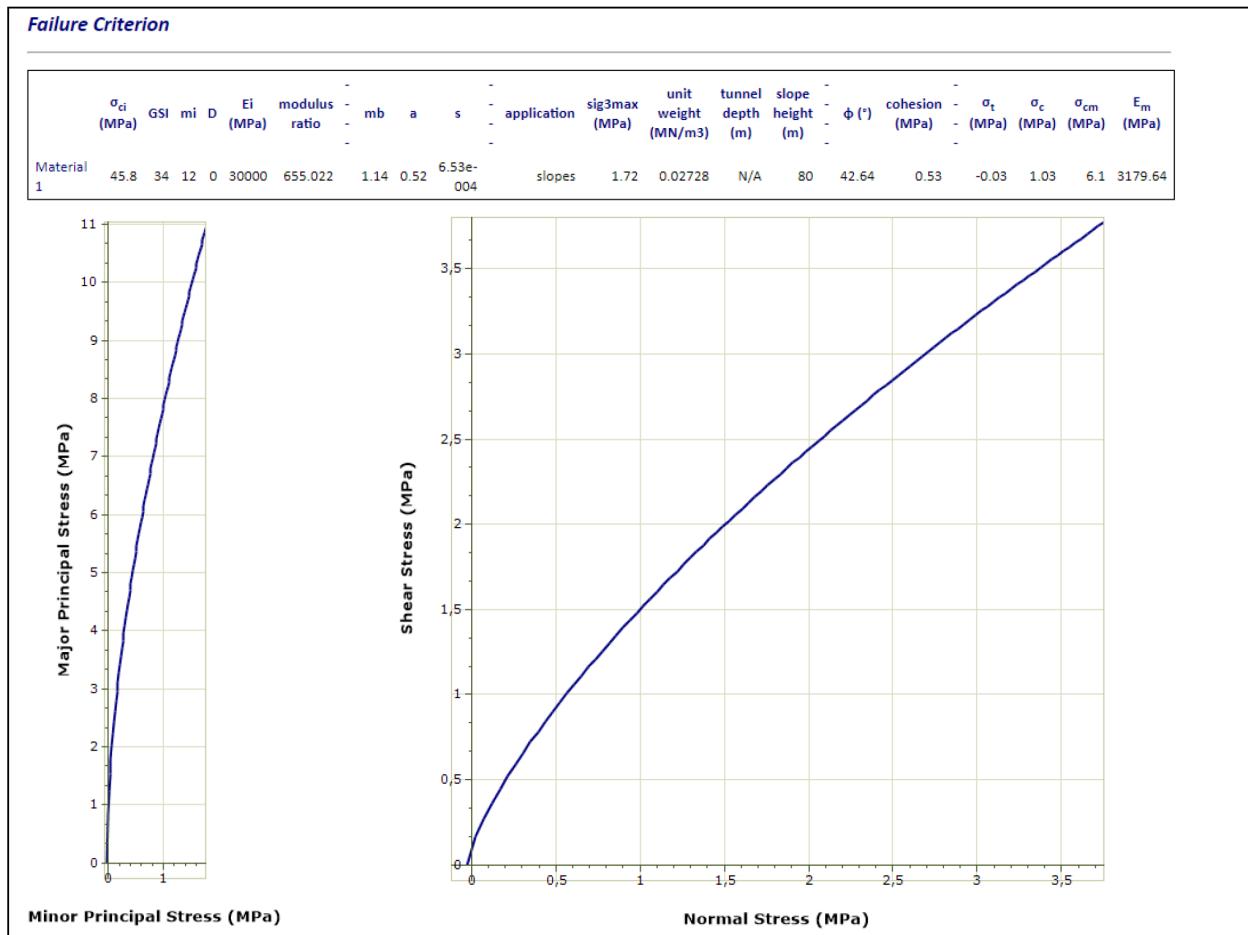
Contour plot of displacement magnitudes [m], 20,000 calculation steps

Number of continuum elements (zones): „before“: 776.620
„after“: 652.463



Used material models

- 1) Mohr-Coulomb (with equivalent parameters)
- 2) Hoek-Brown



Input parameters :

$$\sigma_{ci} = 45,8 \text{ MPa}$$

$$E_i = 30.000 \text{ MPa}$$

$$\text{GSI} = 34 \text{ (Category D)}$$

$$m_i = 12$$

$$D = 0$$

$$\text{Slope height} = 80 \text{ m}$$

Equivalent parameters :

$$\varphi = 42^\circ$$

$$c = 0,5 \text{ MPa}$$

$$\sigma_t = 0,03 \text{ MPa}$$

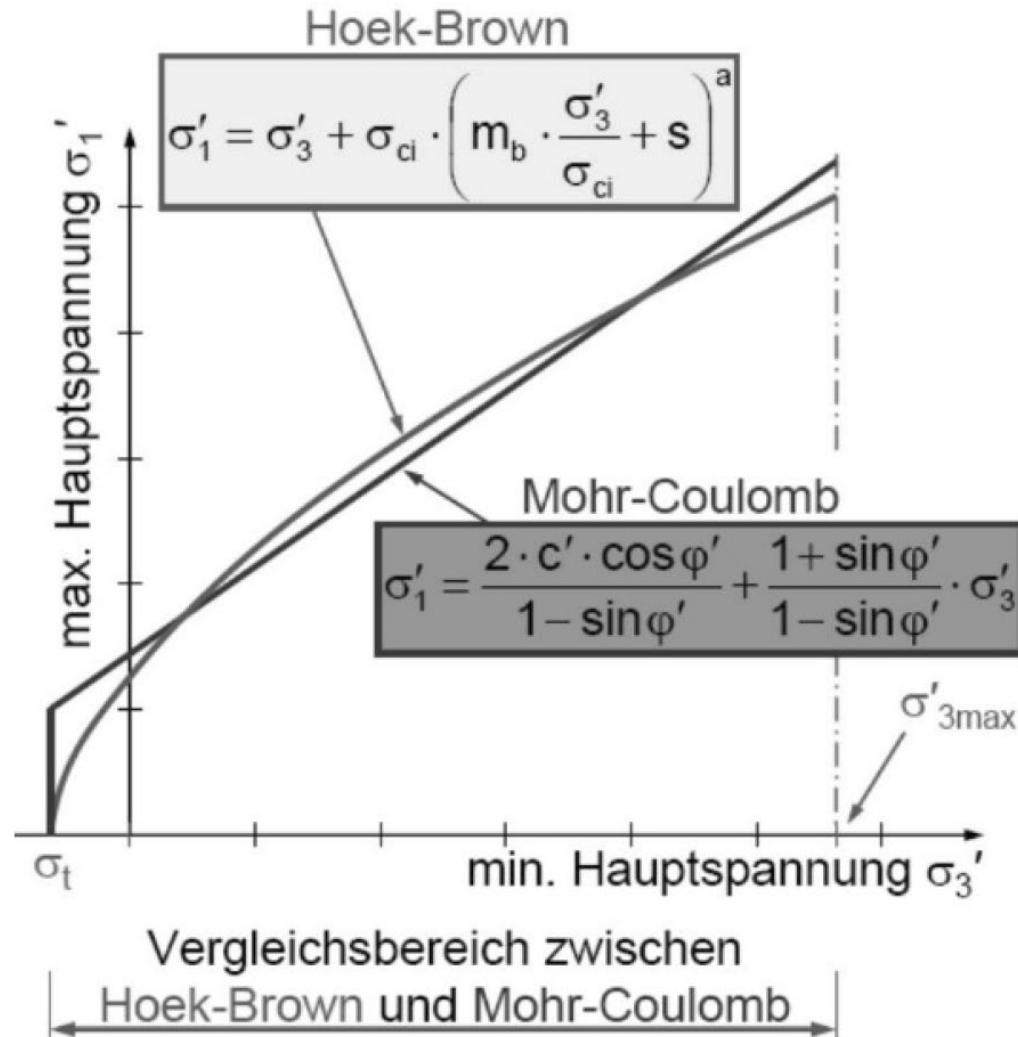
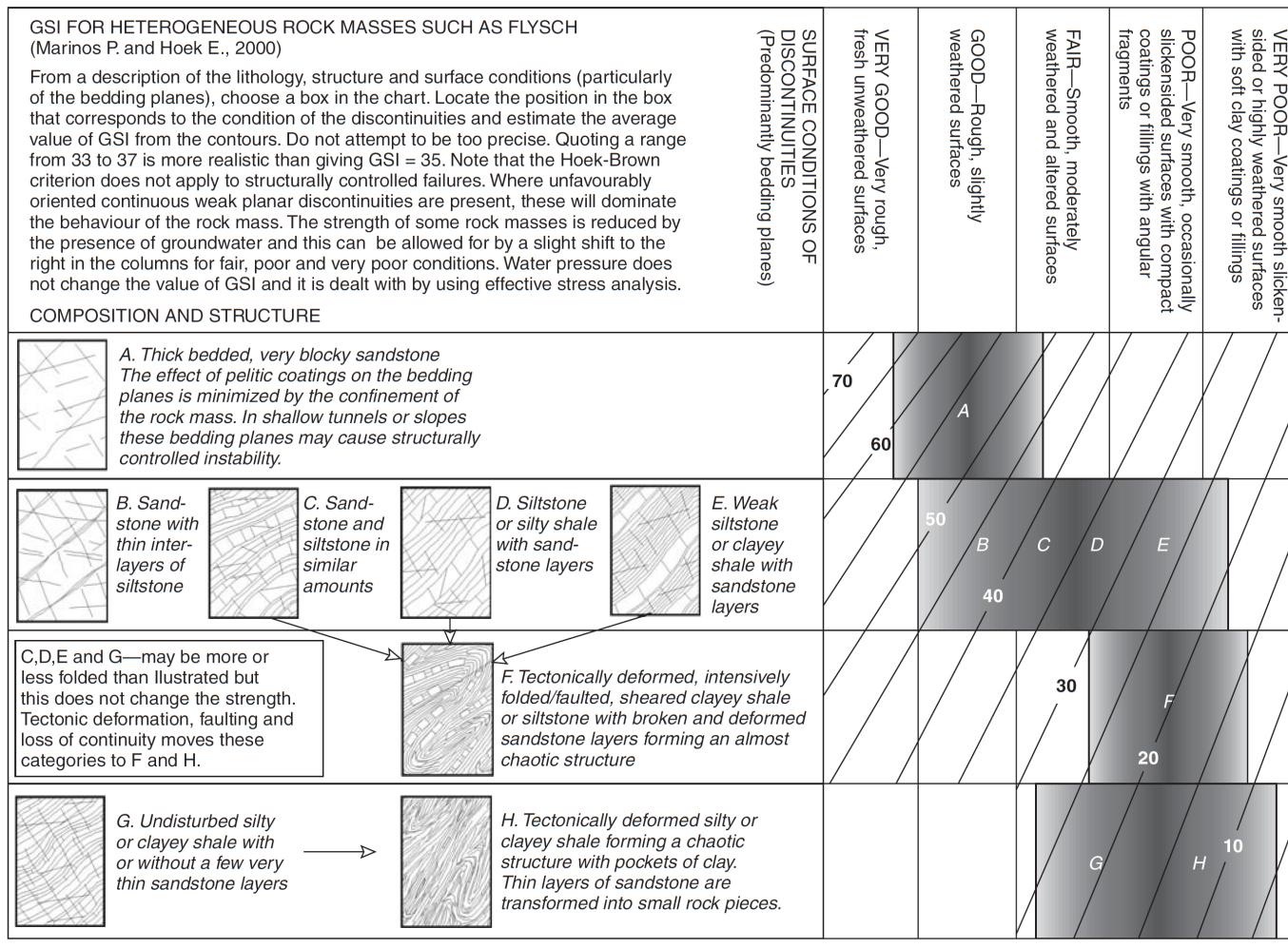
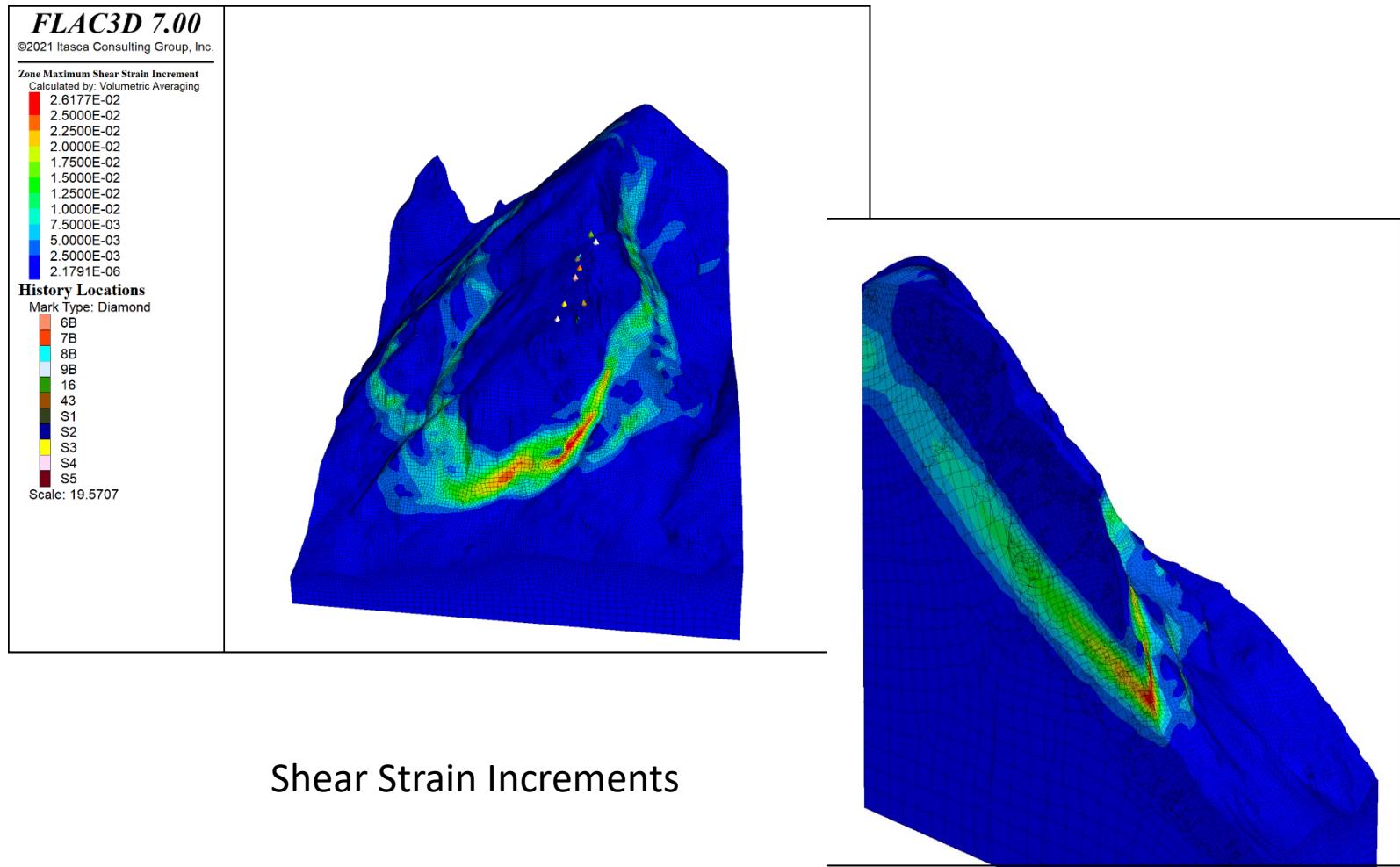


Table 4.4 GSI values characterizing schistose metamorphic rock masses on the basis of foliation and discontinuity condition



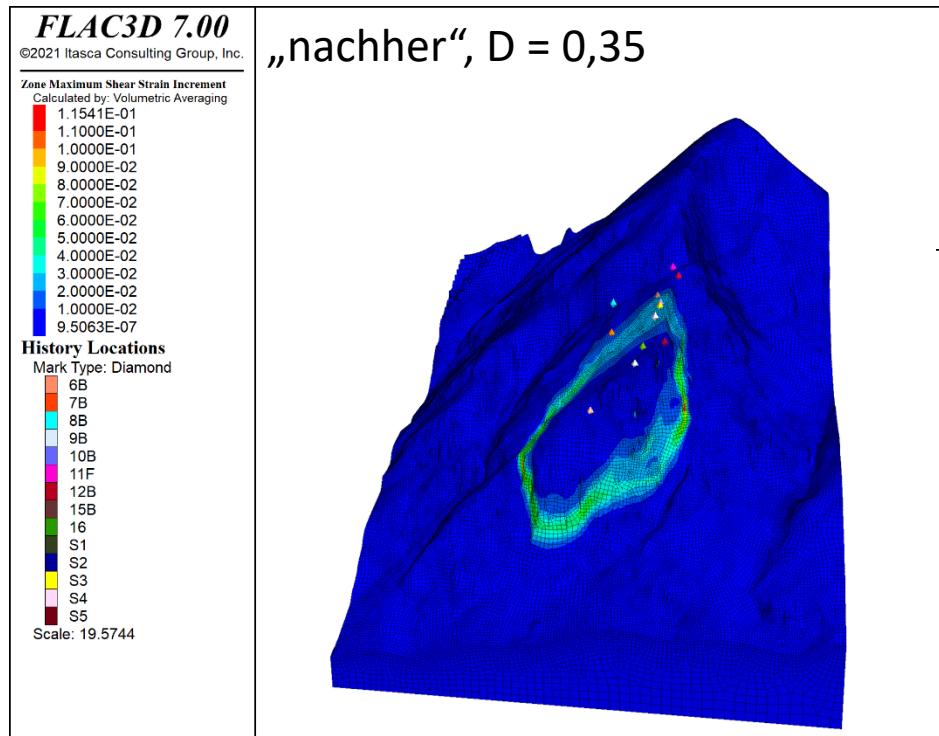
Rock strength properties and their measurement

1) Mohr-Coulomb (with equivalent parameters) - model "after" ($\eta = 1,47$)

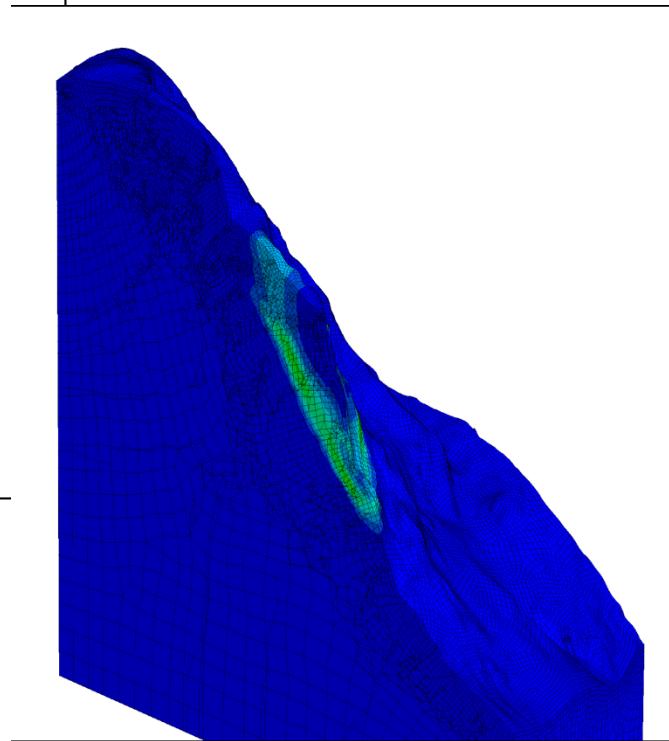


Model calculation after model calibration

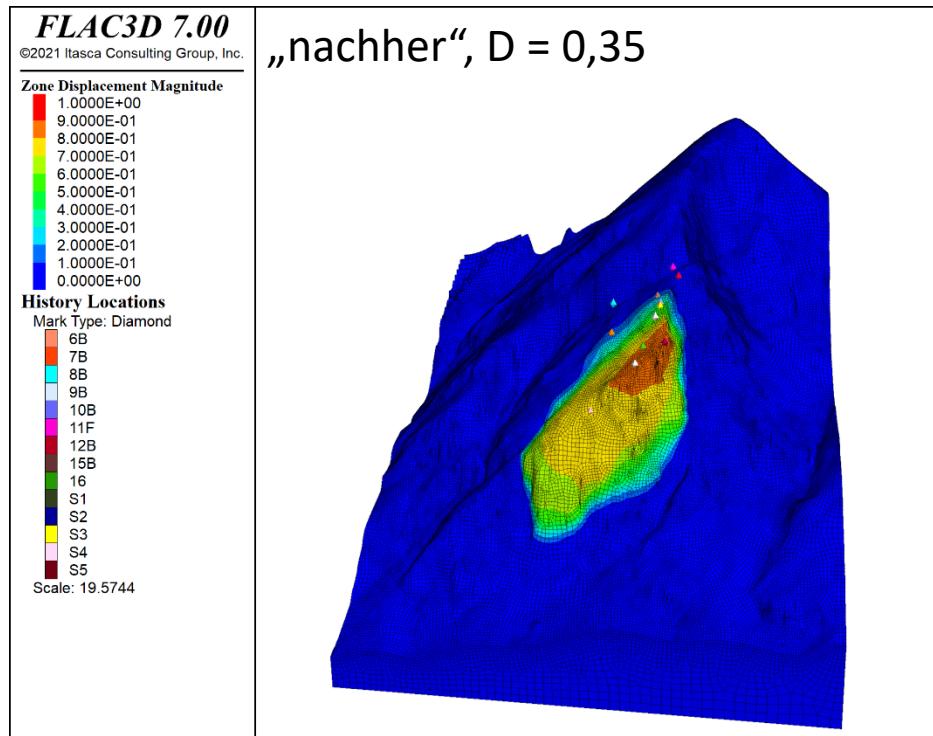
$$\eta = \text{ca. } 1,2$$



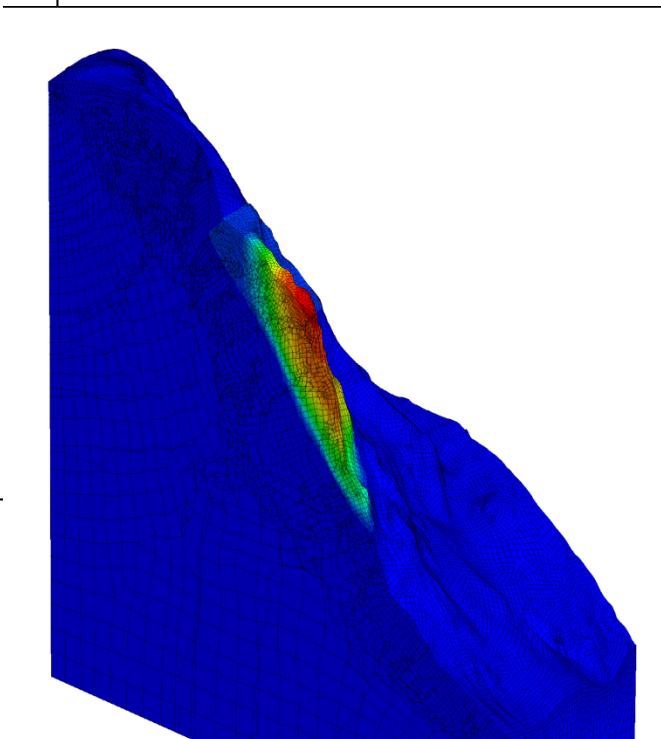
Shear Strain Increments



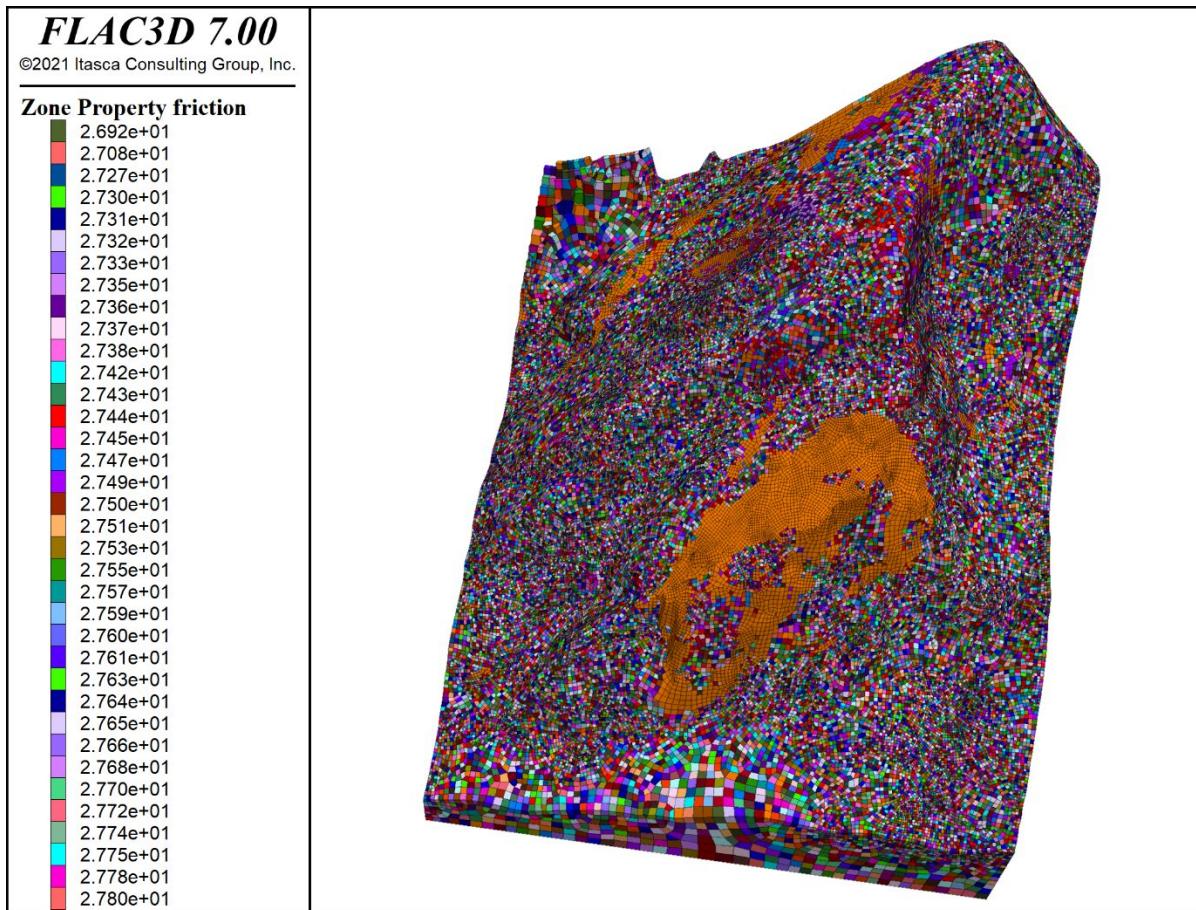
Model calculation after model calibration



Displacement magnitudes [m]



Apperent cohesion and apparent friction



- Every DEM model (including the SRM) requires back-calculations to determine the model parameters.
- Conventional DEM rigid body models shows the best results in discontinuum mechanical models using the back-calculated strengths.
- Continuum mechanics approaches (such as FLAC3D) in combination with the HB material model can provide realistic results.
- Continuum mechanical approaches (such as FLAC3D) in combination with the MC material model are problematic, since the equivalent MC parameters require the estimation of the depth location of the fracture surface.
- Due to the many uncertainties, a combined use of continuum mechanics and discontinuum mechanics is recommended.